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UK CL (Edition J) E1F FLK FLM

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(54) Electrically actuated safety valve for a subterranean well

(57) A downhole safety valve 11 for a subterranean well comprises an axially shiftable valve head which is movable between open and closed positions by an actuating member 20. The actuating member is axially shifted by a device mechanism which is manipulated by an electric motor 30. The electric motor is preferably actuated by downhole batteries 12 and the energization and de-energization of the electric motor is preferably controlled from the well surface by electromagnetic waves. A locking mechanism 40 engages the actuating member of the safety valve in its open position through the energization of an electric solenoid, also preferably controlled from the well surface by electromagnetic waves.

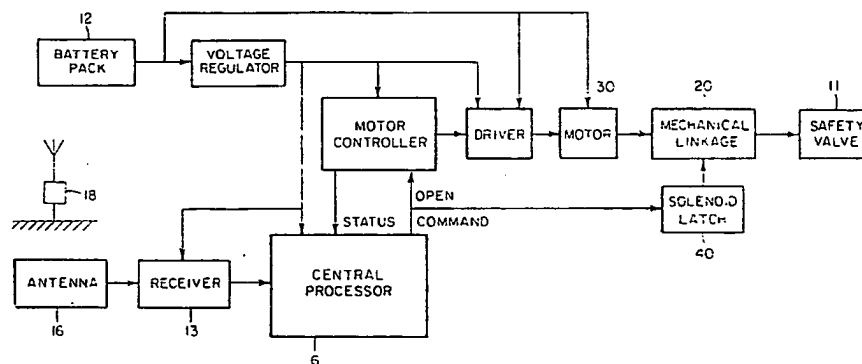
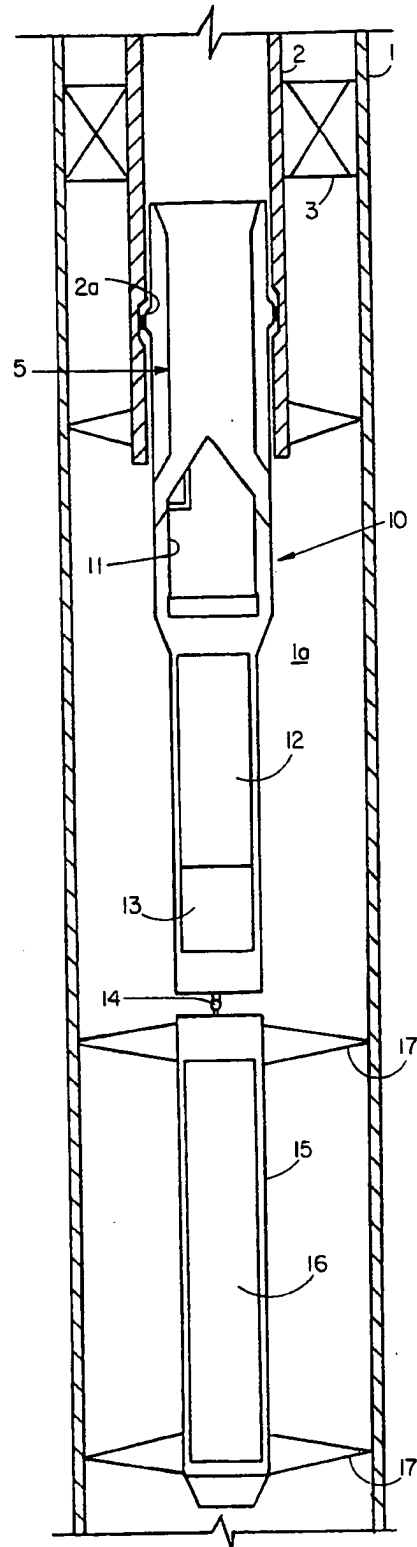


FIG. 4

FIG. 1

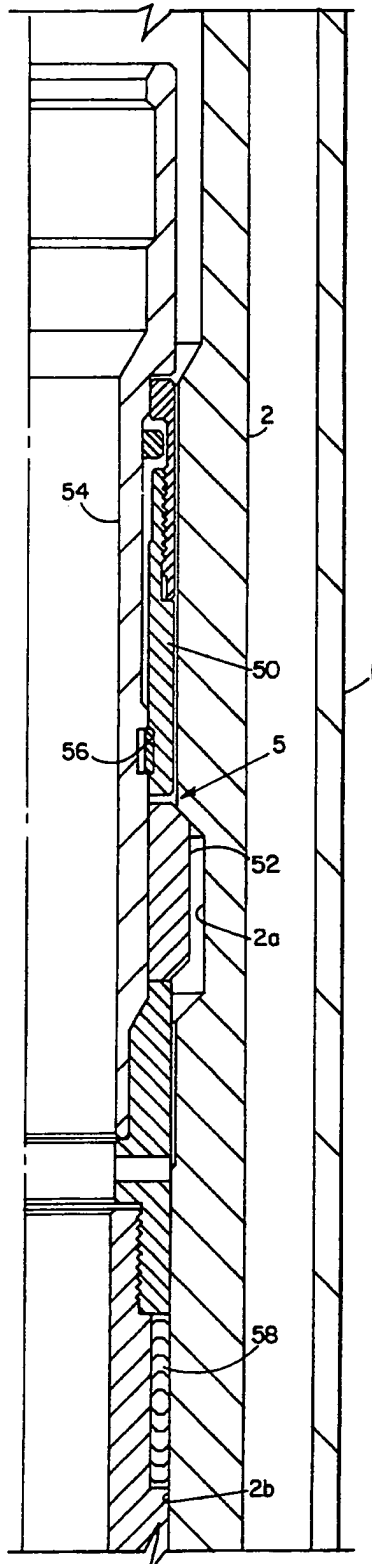


FIG. 2A

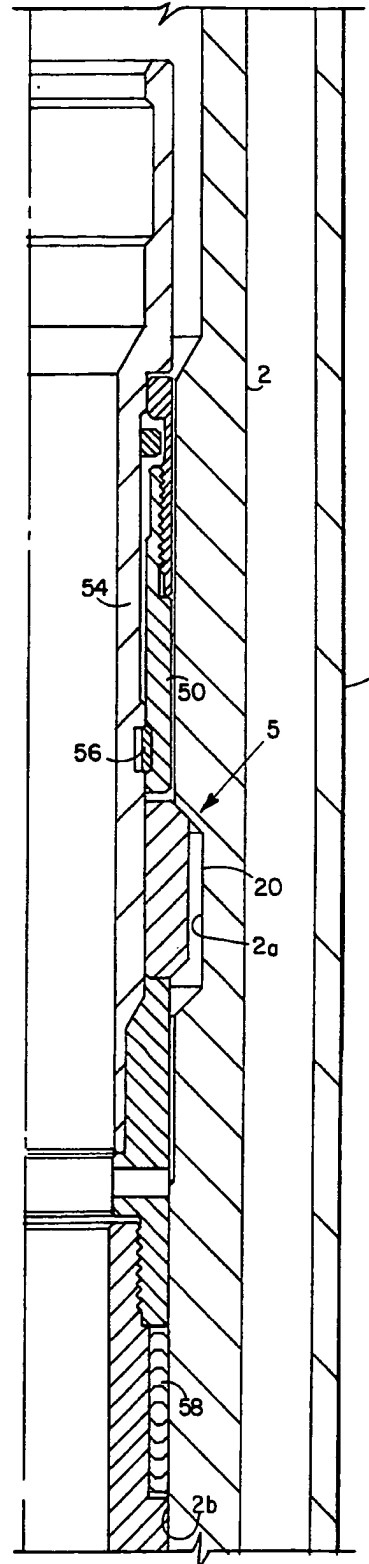
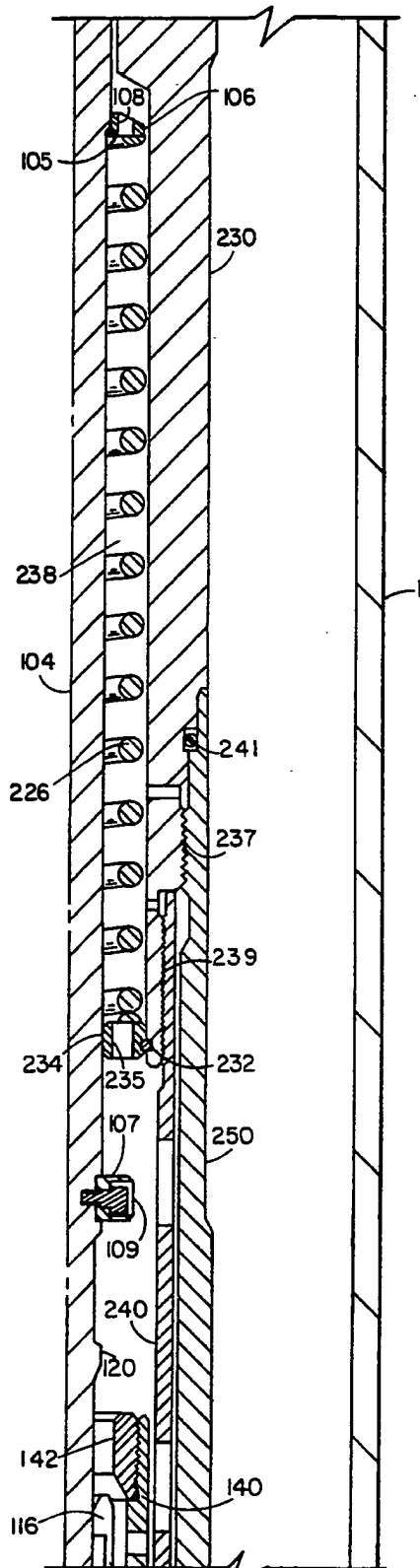
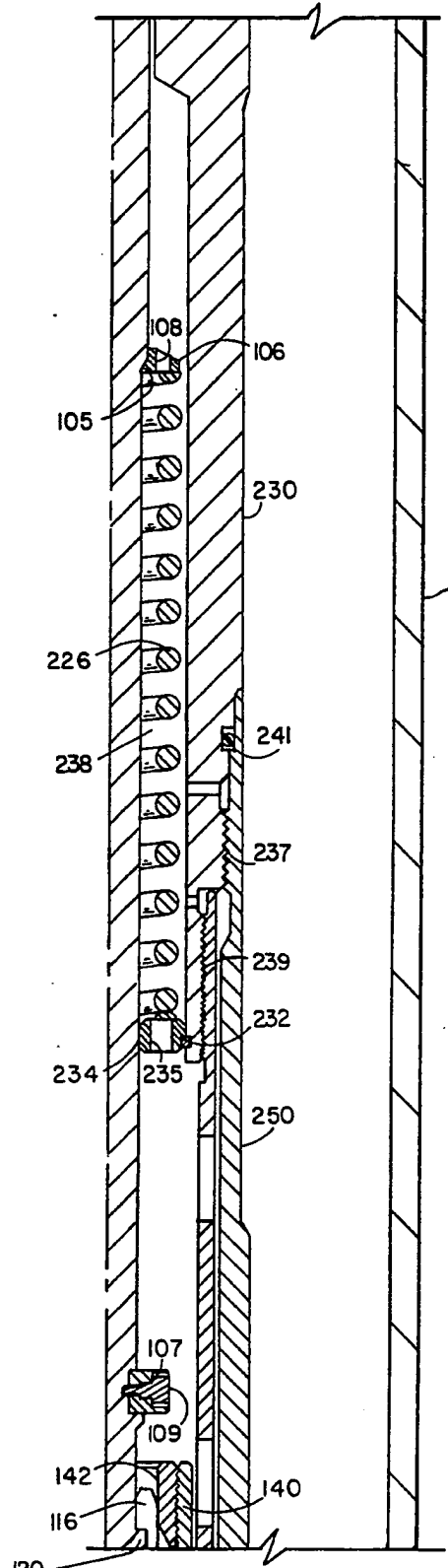
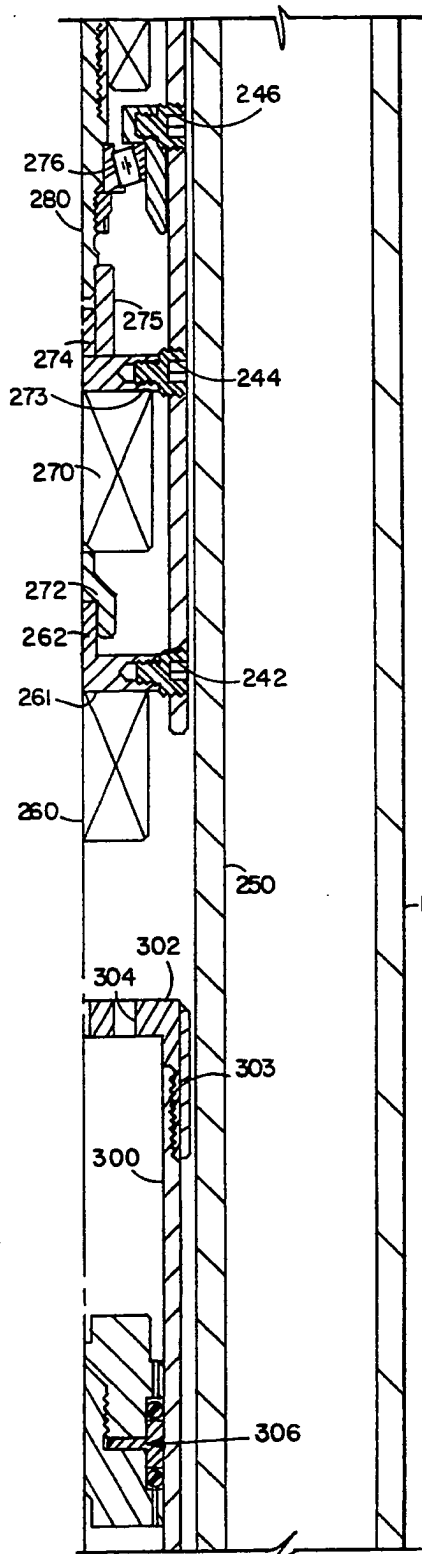
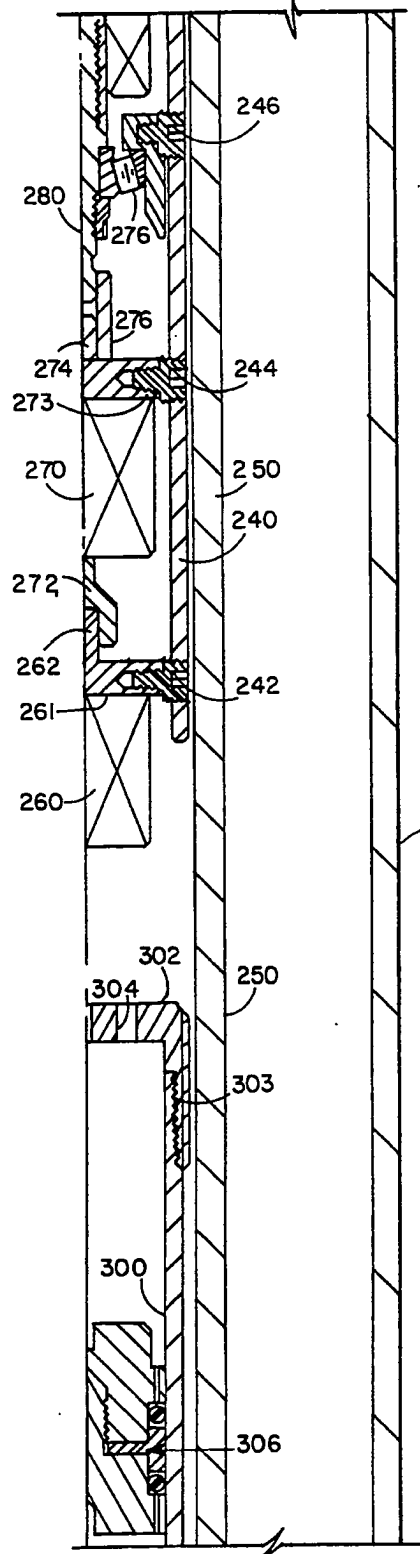


FIG. 3A



**FIG. 2C****FIG. 3C**



**FIG. 2E****FIG. 3E**

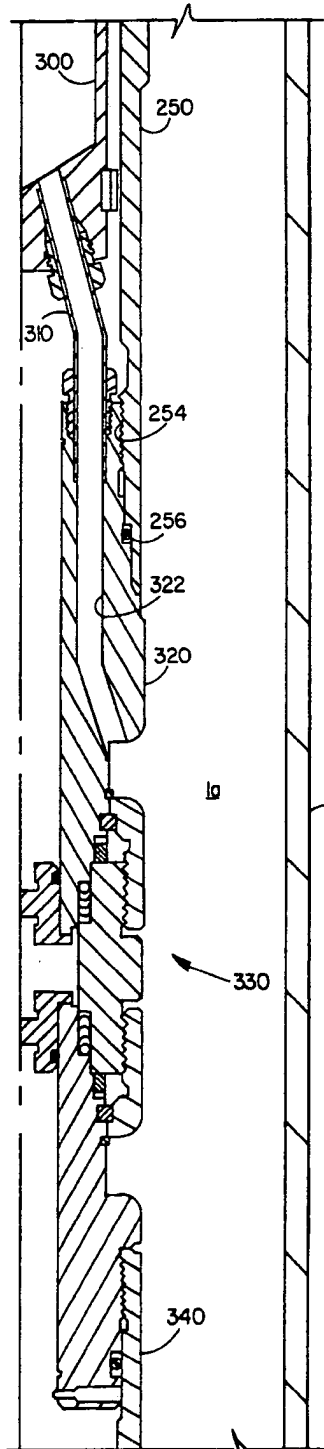


FIG. 2F

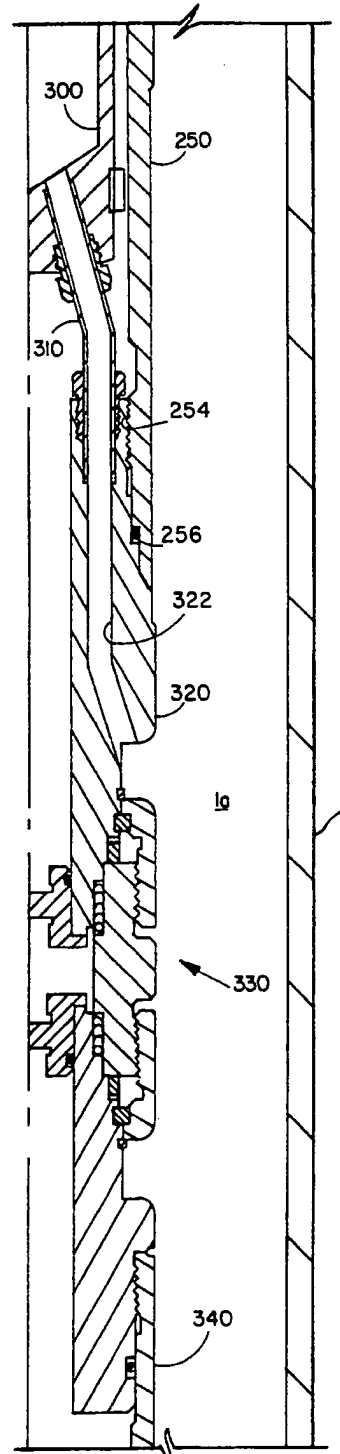


FIG. 3F

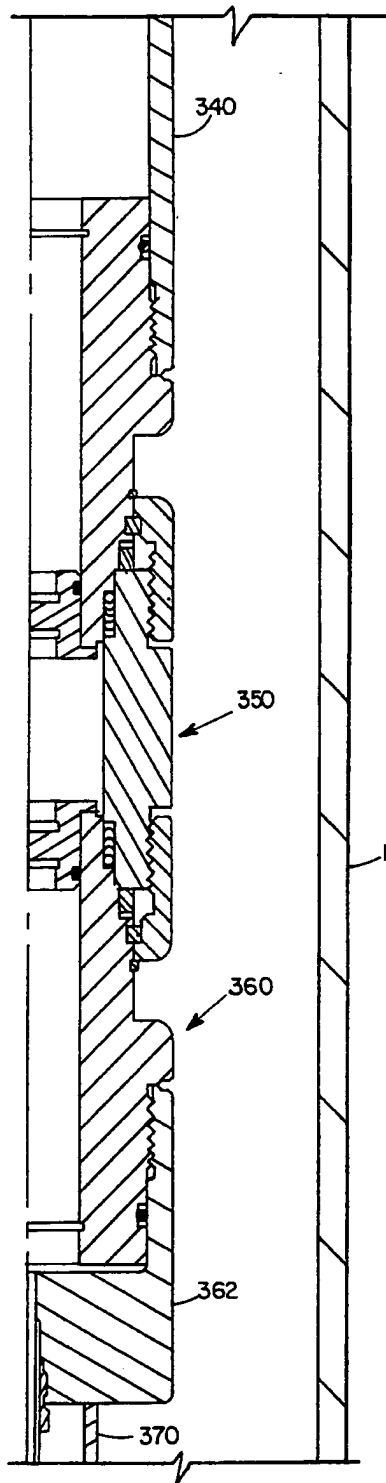


FIG. 2G

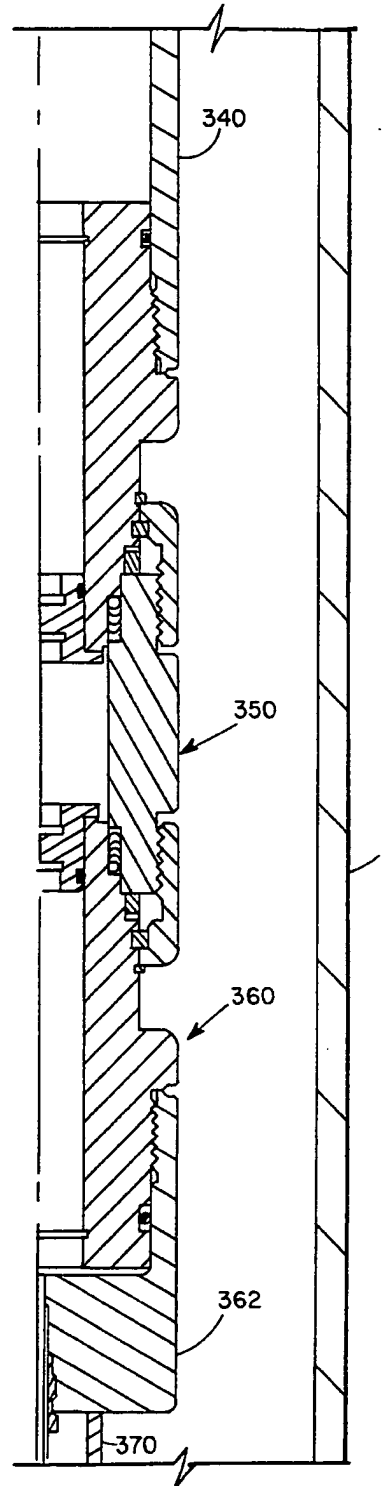


FIG. 3G

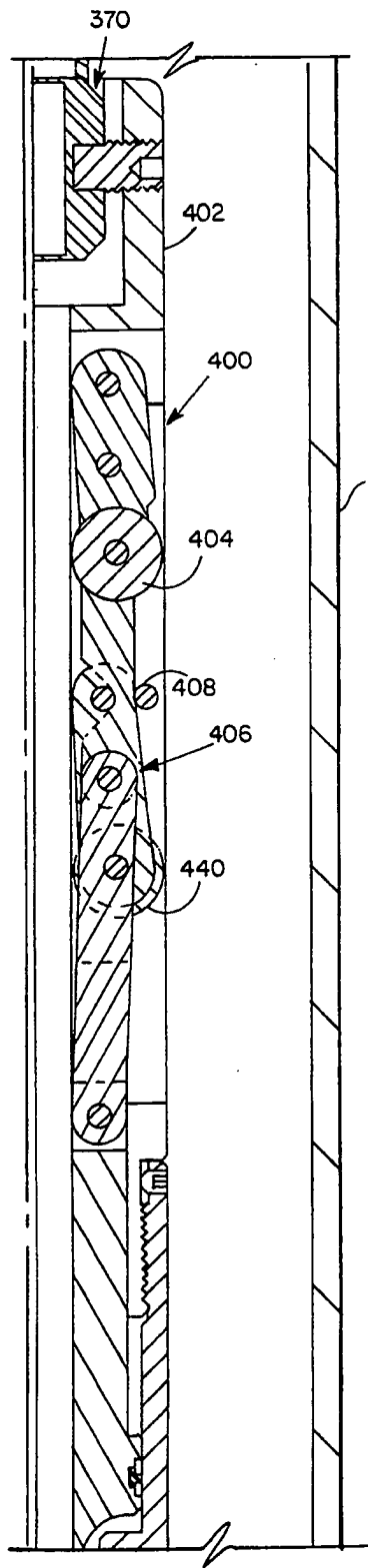


FIG. 2H

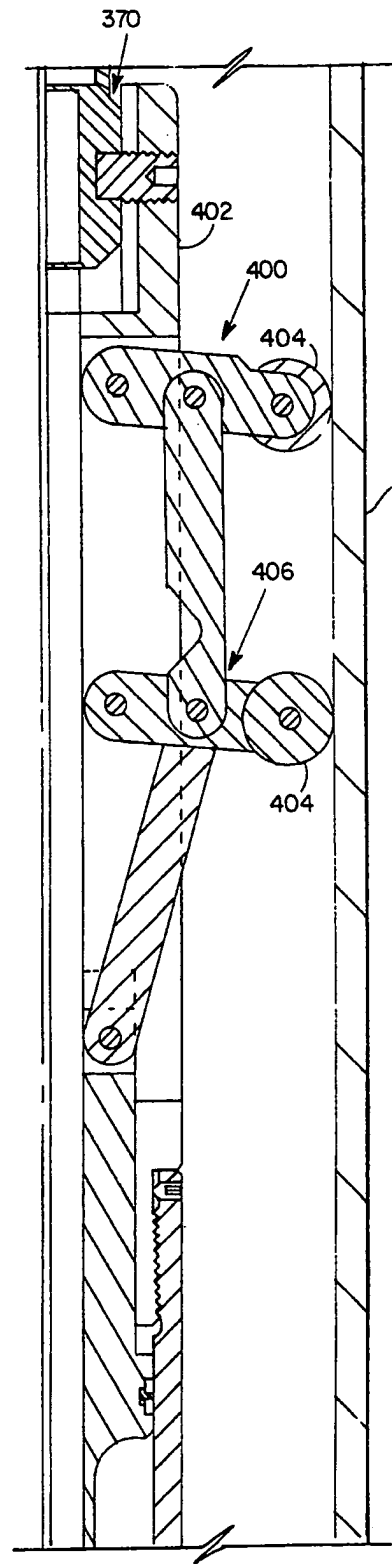


FIG. 3H

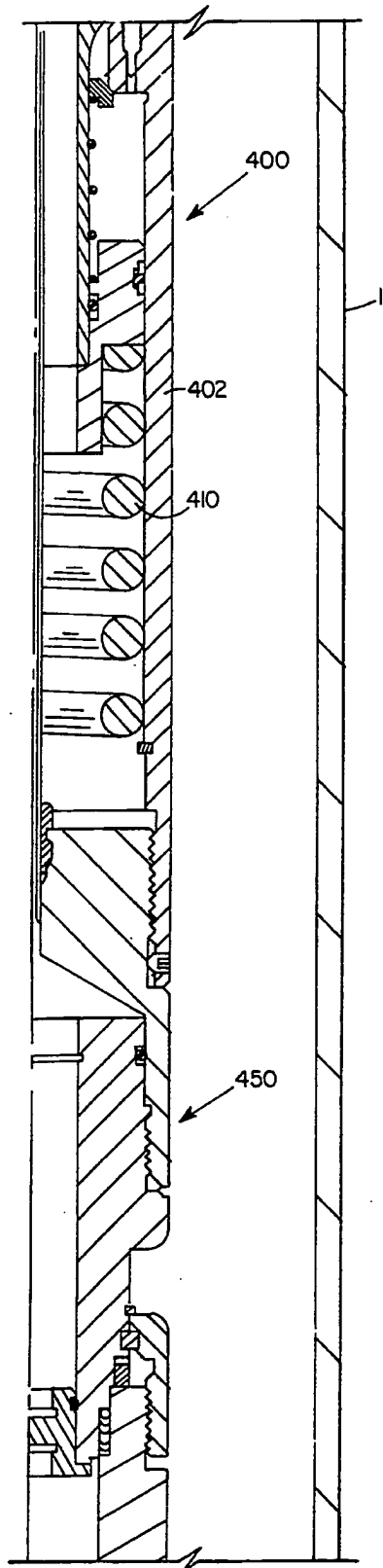


FIG. 2I

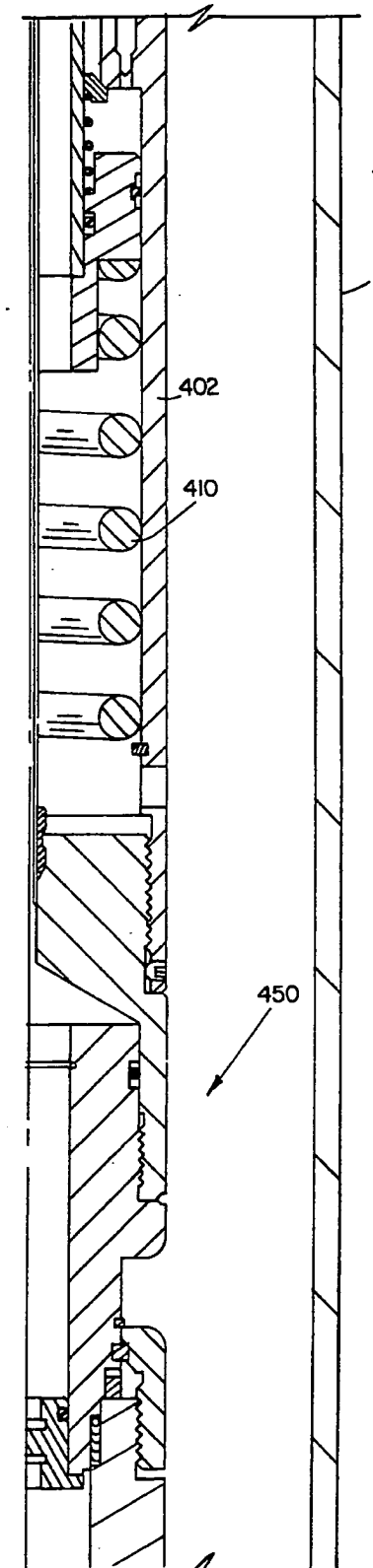


FIG. 3I

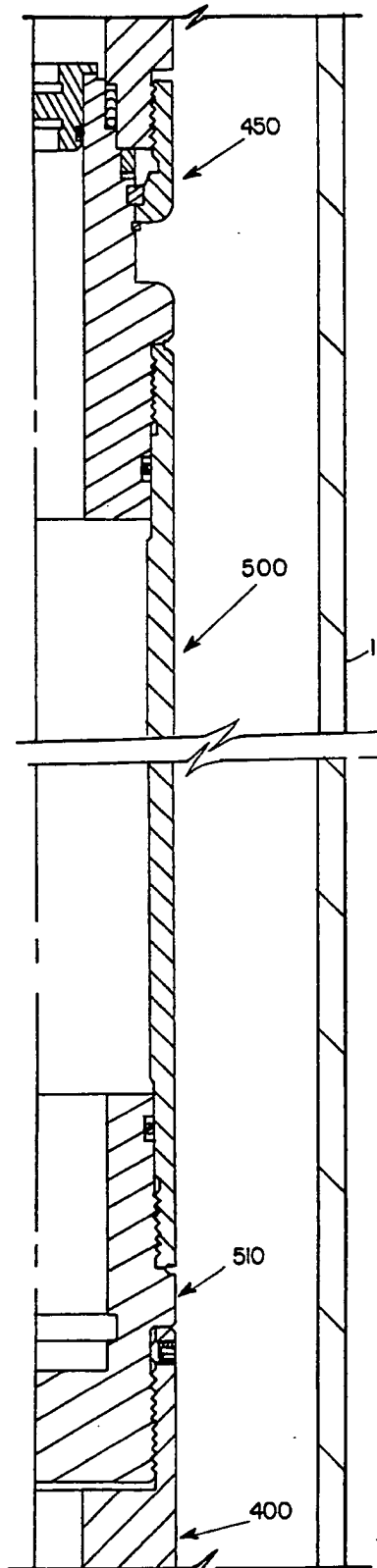


FIG. 2J

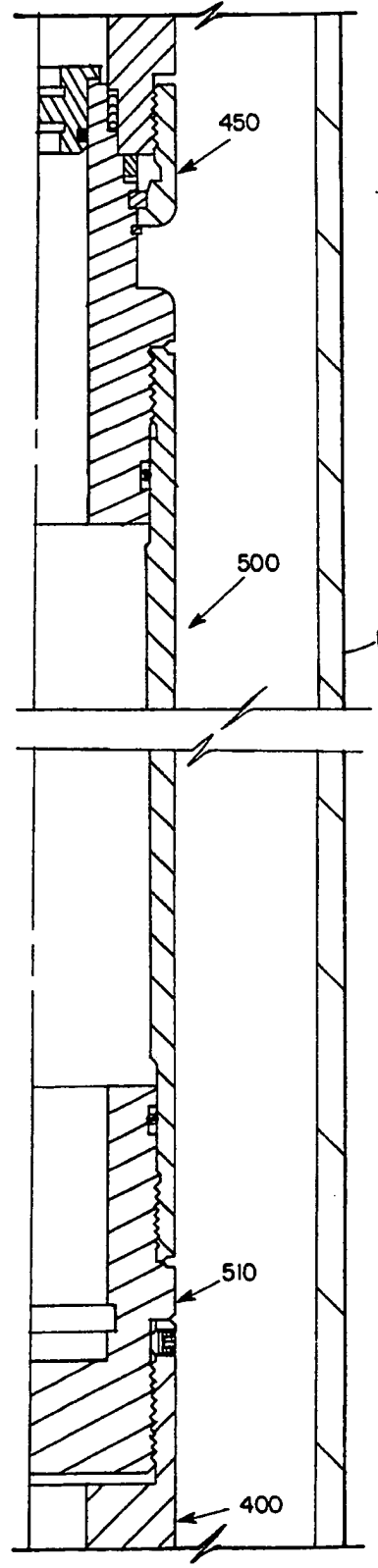


FIG. 3J

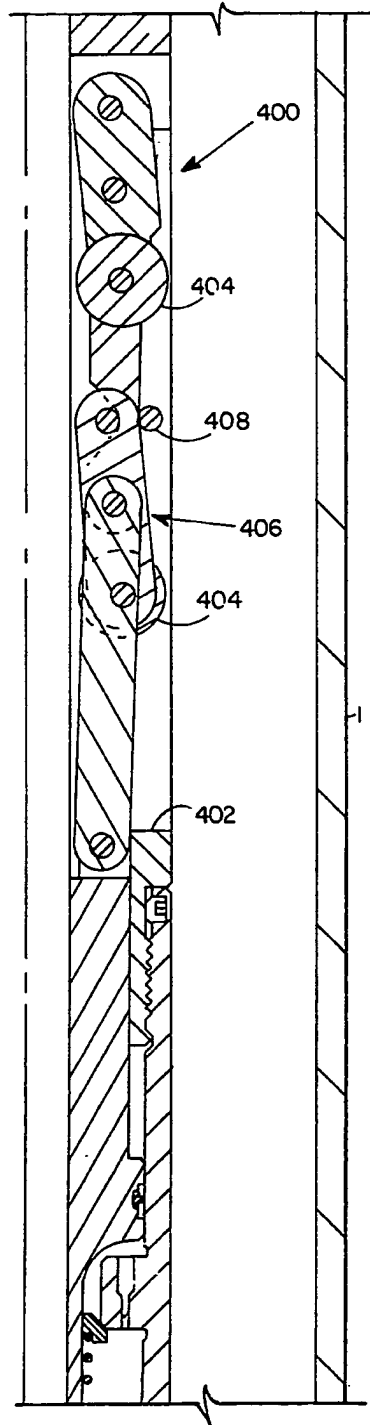


FIG. 2K

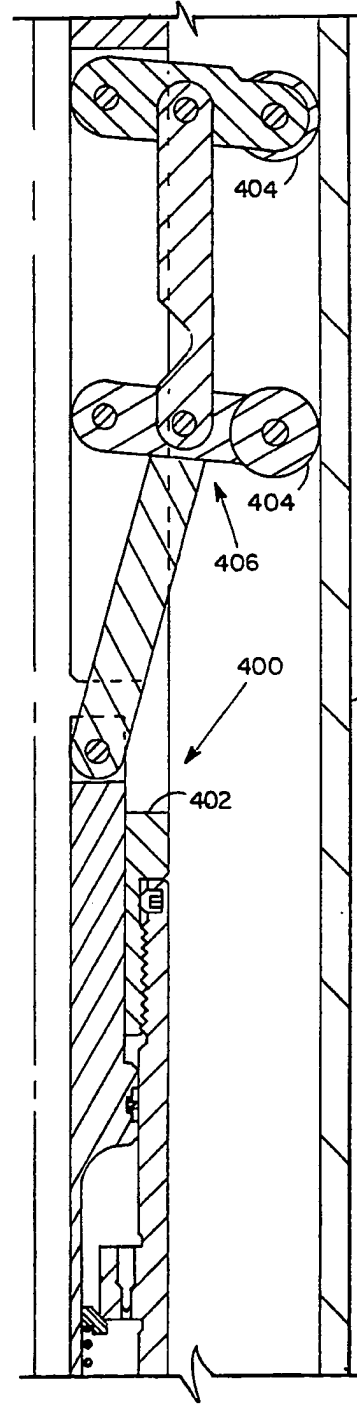
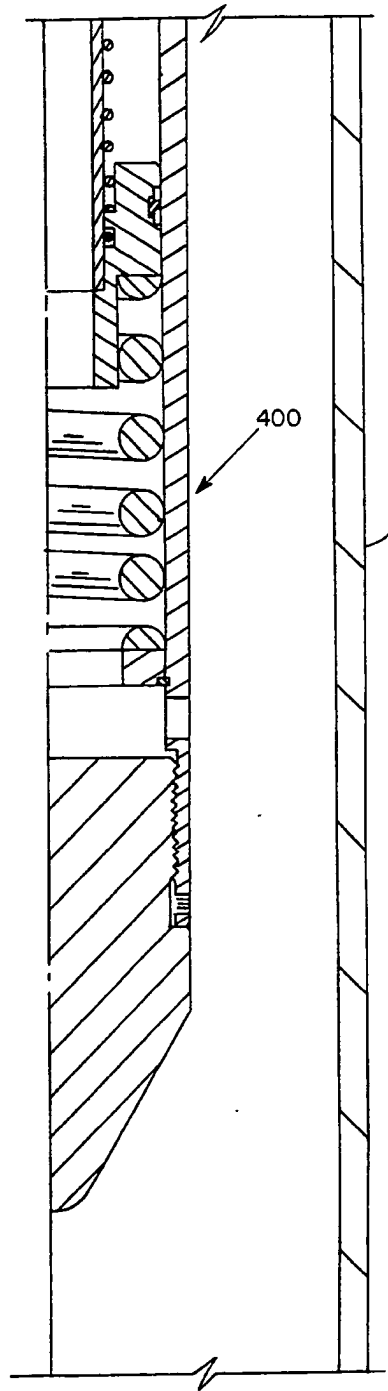
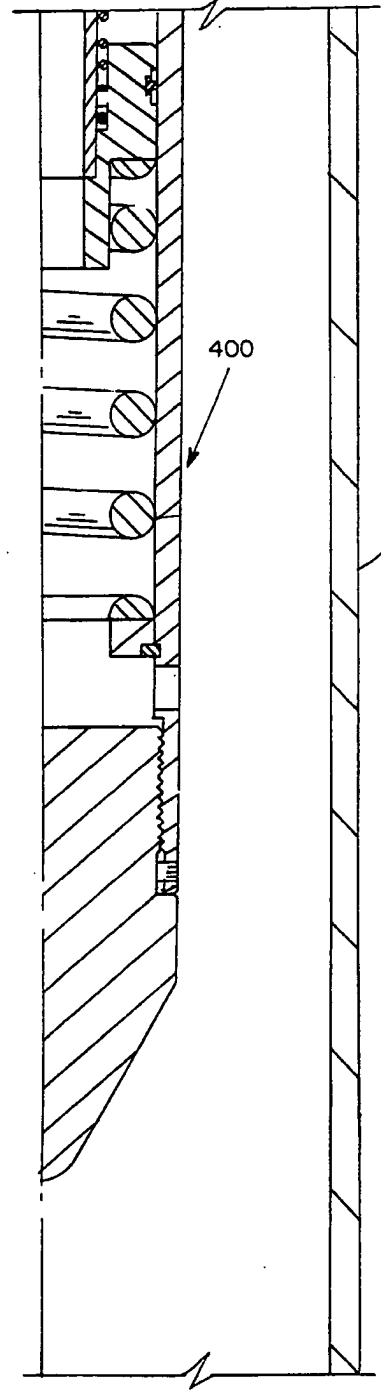
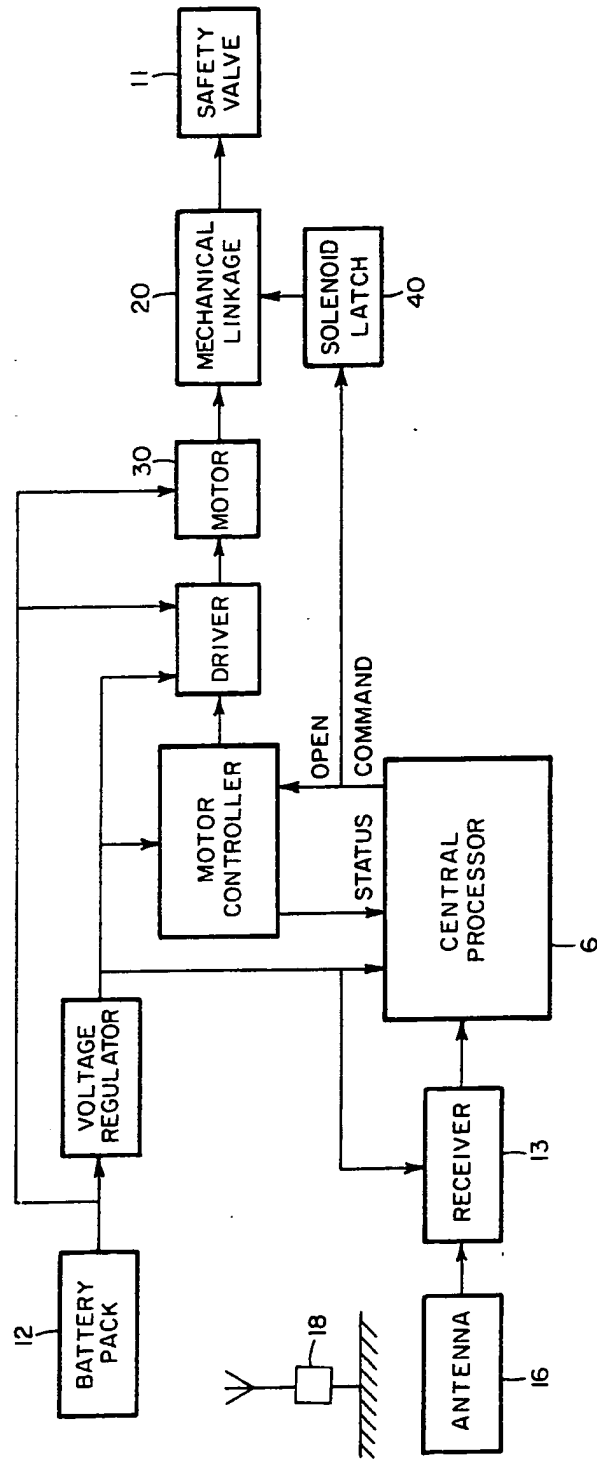


FIG. 3K

FIG. 2LFIG. 3L

**FIG. 4**

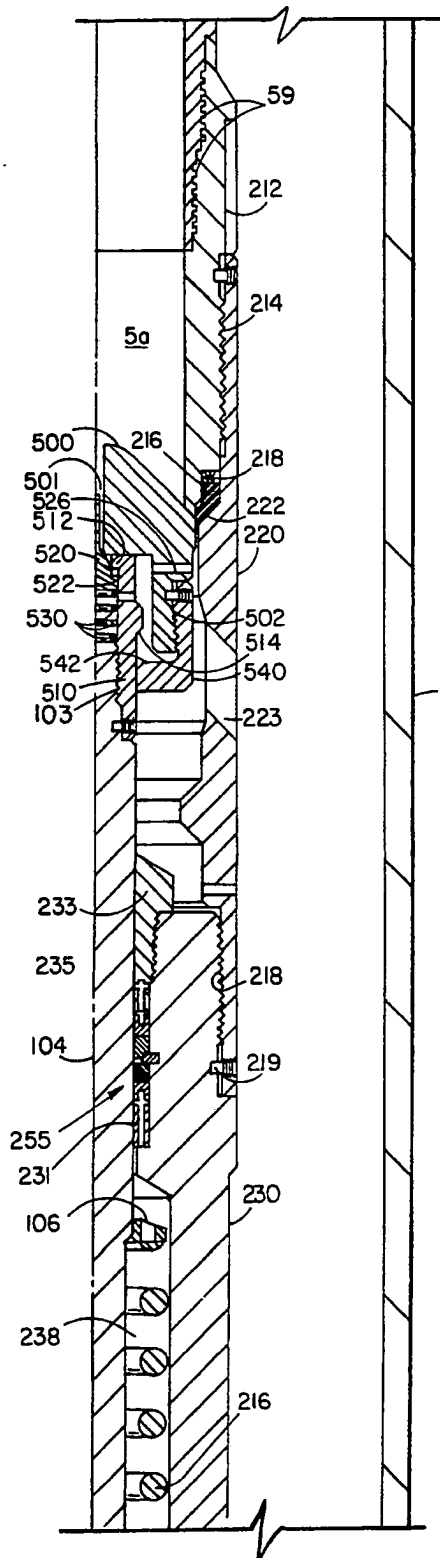


FIG. 5A

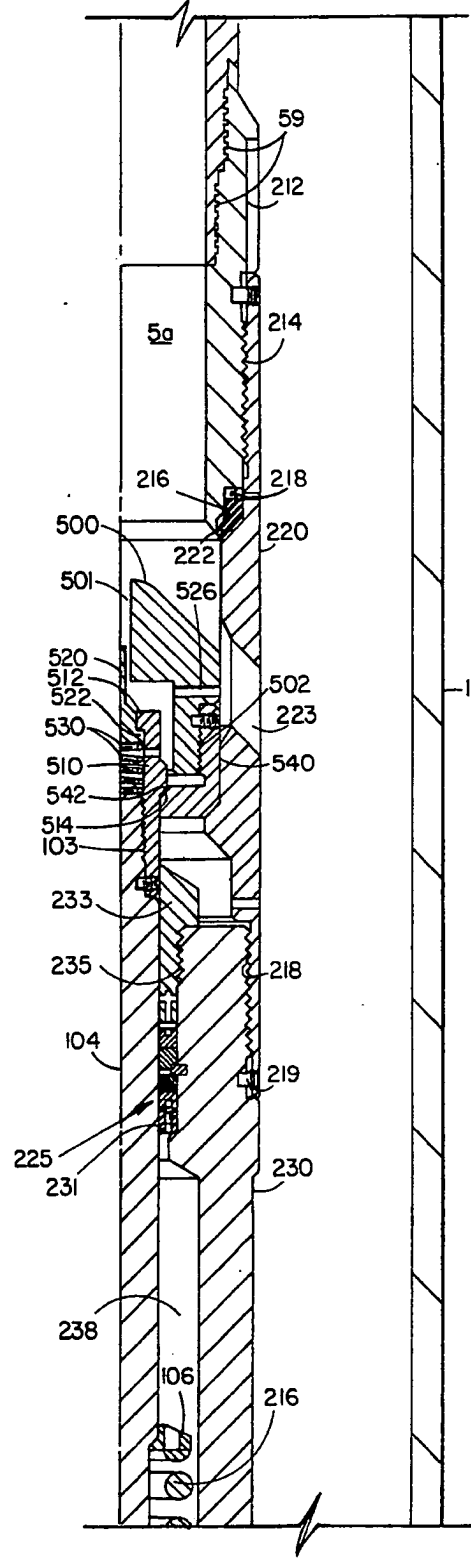


FIG. 5B

Electrically Actuated Safety Valve for a
Subterranean Well

The invention relates to
a downhole safety valve for a subterranean well, and more
5 particularly to a safety valve utilizing electrical mechanism,
controlled from the surface by electromagnetic waves, for
opening and closing the valve and for locking the valve in an
open position.

The employment of a
10 downhole safety valve is well known for subterranean oil and
gas wells. Such valve, which can comprise a plug or poppet
type, a sleeve valve, a flapper valve, or a ball valve, is
normally positioned downhole to close the bore of the tubing
string leading from one or more production zones to the well
15 surface. Such safety valves are normally biased to a fail
safe condition, i.e., energized means will shift the valve to
its closed position upon any significant reduction in the
opening force applied to the valve structure.

The more common type of safety valves utilizes a
20 control fluid pressure to effect the shifting of the valve to
its open position. Such control fluid pressure is supplied
through a small control conduit which is run into the well
concurrently with the production tubing. Necessarily, such
conduit is susceptible to damage during the run-in process, or
25 joints in the conduit may develop leaks. In any event, the
loss of integrity of the conduit will effect the immediate
closing of the safety valve and the well is essentially out of
operation until the entire tubing string has been pulled from
the well and the necessary repairs made.

1 To offset the difficulties involved in the utilization
of a control pressure conduit, it has been previously proposed
that the downhole safety valve be actuated from its closed to
its open position by a downhole solenoid which is supplied with
5 electrical power from the surface by an electric line. The
same problem of potential damage to the electric line during
the run-in process exists with this arrangement and, of course,
any abrasion of the insulation of the electric line during the
run-in process leads to the possibility of short circuits de-
10 veloping in the electric line, again requiring that the entire
tubing string be pulled from the well to effect the necessary
repairs.

 It is often necessary to run tools down through the
production conduit and the open downhole safety valve to effect
15 treatment of the production formation. Under such conditions,
it is highly desirable that the safety valve be positively
locked in an open position so that unexpected fluctuations in
well pressure will not cause the safety valve to attempt to
close when a wireline or a treatment conduit is passing through
20 the valve. A variety of fluid pressure or mechanically actuated
latching mechanisms have heretofore been proposed to effect the
locking of a downhole safety valve in an open position. U.S.
Patent 4,579,177 discloses a solenoid actuated locking mecha-
nism for a downhole safety valve. Such solenoid is energized
25 by an electric line leading to the well surface, hence is
subject to the problems mentioned above involved in maintaining
the integrity of an electric line run into a subterranean well
concurrently with production tubing.

 There is a need, therefore, for a subsurface safety
30 valve which is controllable from the surface to move from a

1 closed to an open position, and also incorporates a locking
mechanism, controllable from the well surface, for selectively
maintaining the safety valve in a locked-open position, which
does not depend upon the utilization of a control fluid pres-
5 sure conduit or an electric line extending from the safety
valve to the well surface to effect its operation.

In recent years, systems have been developed for
transmitting relatively low frequency electromagnetic waves
through ground or water by launching and propagating magnetic
10 waves of generally vertical magnetic polarization through the
intervening subterranean region of earth or water between a
pair of magnetic dipole antennas. See, for example, U.S.
Patent 3,967,201 to RORDEN.

In co-pending application, Serial No. 730,397, filed
15 May 3, 1985, entitled "Improvements in Subsurface Device
Actuators," and assigned to a wholly owned subsidiary of the
assignee of the instant application, there is disclosed a
system for actuating a downhole safety valve between open and
closed positions in response to low frequency electromagnetic
20 waves received by a downhole antenna from a surface located
transmitting antenna. Such apparatus incorporates a downhole
battery but does not employ the battery for effecting the
shifting of the safety valve from its closed to its open posi-
tion, an act which requires a substantial amount of electrical
25 energy. Instead, the system disclosed in such application
relies upon fluid pressure to effect the shifting of the safety
valve from a spring bias closed position to an open position.

Such co-pending application does, however, disclose a
downhole battery and a locking solenoid selectively energized
30 by such battery in response to electromagnetic wave signals

generated by a surface transmitter. The energization of the solenoid effects the operation of a locking mechanism to secure the safety valve in its open position. Thus, while some of the disadvantages of the above described prior art systems have been overcome, the construction disclosed in the aforesaid pending application still requires the utilisation of fluid pressure to effect the shifting of the safety valve to an open position.

This invention provides apparatus for shifting a downhole tool axially shiftably mounted in a subterranean well conduit for movement between an initial and a second position comprising,

an axially extending actuator connected at one end to the downhole tool;

resilient means opposing axial movement of the actuator in the direction away from the initial position;

peripheral abutment means on the actuator;

shifting means disposed adjacent the actuator;

an axial force transmitting member in operative engagement with the shifting means;

means for mounting the force transmitting member for non-rotatable axial movement relative to the conduit;

an electric motor fixedly mounted in the conduit;

and threaded means rotatable by the electric motor and threadably engageable with the force transmitting member to axially shift the shifting means and the actuator in the direction opposed by the resilient means and thereby position the downhole tool in the second position.

Typically the downhole tool is a downhole safety valve in a subterranean well, which has an axially shiftable actuator which is moved by an electric motor driven drive mechanism between opening and closing positions of the safety valve. The safety valve may comprise any one of the well known types, namely a poppet

valve, a sleeve valve, a flapper valve, or a ball valve, the only requirement being that such valve be capable of being opened by axial movement of an actuator. The electric motor for effecting the axial shifting of the
5 actuator is energised by a downhole battery and the energization of the motor to rotate in either direction is selectively controlled by electromagnetic wave signals generated at the well surface.

Additionally, this invention may provide a locking
10 mechanism for effecting the locking of the safety valve in its open position. Such locking mechanism is actuated by the battery energization of a solenoid. Again, the selective energization of such solenoid is controlled by electromagnetic waves transmitted from the
15 well surface.

Moreover, the apparatus of this invention preferably employs a fail safe means to effect the return of the safety valve from its open to its closed position, thus eliminating _____

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1 any drain on the battery to effect the closing stroke of the
valve. The only energy required to maintain the valve in its
locked open position is that required by the solenoid which is
minimal, due to the fact that the armature of the solenoid only
5 has to retain a relatively light weight latch retaining sleeve
in engagement with collet arms which are lockingly engaged with
the actuator for the safety valve. Thus, the necessity of
providing a continuous high current to maintain the safety
valve in an open position has been eliminated.

10 Lastly, a pressure equalizing mechanism is provided
for the safety valve which is actuated by the initial axial
movement of the actuator from its valve closing position.

Thus, the method and apparatus of this invention
provides a conveniently controllable downhole safety valve
15 which may be selectively opened or closed by electromagnetic
waves transmitted from the well surface and eliminates the
necessity of running either control fluid conduits or electric
wires into the well solely for the purpose for controlling the
operation of the safety valve.

20 Further objects and advantages of the invention will
be readily apparent to those skilled in the art from the fol-
lowing detailed description, taken in conjunction with the
annexed sheets of drawings, on which is shown a preferred
embodiment of the invention.

25 Figure 1 is a schematic vertical sectional view of a
safety valve embodying this invention shown in its installed
position within a production conduit of a subterranean well.

30 Figures 2A, 2B, 2C, 2D, 2E, 2F, 2G, 2H, 2I, 2J, 2K
and 2L collectively constitute a schematic vertical sectional

1 view illustrating the detailed construction of a safety valve
embodying this invention installed in a subterranean well, with
the elements of the safety valve shown in their closed position.

5 Figures 3A, 3B, 3C, 3D, 3E, 3F, 3G, 3H, 3I, 3J, 3K,
and 3L are views respectively similar to Figures 2A, 2B, 2C,
2D, 2E, 2F, 2G, 2H, 2I, 2J, 2K and 2L but showing the elements
of the safety valve in their locked open position.

Figure 4 is a schematic diagram of the control circuit
for the safety valve embodying this invention.

10 Figure 5A is a sectional view of a safety valve
embodying this invention and incorporating a pressure equalizing
feature with the valve in its closed position.

Figure 5B is a view similar to Figure 5A but with the
valve shown in its open position.

15 Referring first to the schematic view of Figure 1, a
housing 10 for a safety valve embodying this invention is shown
installed in the bottom end of production tubing 2 which is run
into a well casing 1. The annulus 1a between the production
20 tubing 2 and the well casing 1 is sealed by a conventional
packer 3. The safety valve housing 10 may be suspended in the
bottom end of the production tubing string 2 by any type of
conventional latching mechanism 5 which cooperates with an
internal recess 2a formed in the production tubing 2.

25 Safety valve housing 10 incorporates a safety valve
mechanism 11, a battery case 12, and an electronic signal con-
verter unit 13. An antenna housing 15 is flexibly connected to
the bottom end of the safety valve housing 10 by a conventional
flex joint 14 and houses an antenna 16. The antenna housing 15
30 maintained in a fixed axially aligned position relative to the

axis of casing 1 by a pair of stabilizing units 17 respectively mounted at either end of the antenna housing 15.

As best shown in the schematic circuit diagram of Figure 4, a surface mounted electromagnetic wave transmitter 18 transmits an electromagnetic signal downwardly through the earth which is received by antenna 16 and supplied to an electronic receiver unit 13. The transmitter 18 and receiving antenna 16 may be of the type described in said co-pending application Serial No. 730,397. Electronic unit 13 receives and amplifies the received signal and supplies it to a central processor unit 6. Processor 6 in turn controls the supply of energy from the batteries in battery case 12 to a motor 30 for effecting the shifting of a safety valve actuator 20 between open and closed positions. Additionally, the processor unit 6, in response to a second signal carried by the electromagnetic waves generated by transmitter 18 selectively applies energy to a solenoid latch 40 (hereinafter described) to selectively effect the locking of the safety valve 11 in an open position.

Referring now to Figures 2A, 2B, 2C, 2D, 2E, 2F, 2G, 2H, 2I, 2J, 2K and 2L the detailed mechanism constituting the apparatus of this invention will be described.

Referring specifically to Figures 2A and 2B, the safety valve housing 10 is secured within the bottom end of production tubing string 2 by a conventional latching mechanism 5 including a tubular latching body 50 in which are mounted a plurality of peripherally spaced, radially shiftable latching dogs 52 which are respectively held in engagement with an internal recess 2a in production tubing 2 by a wireline actuated sleeve 54. When the latch 5 is engaged, the sleeve 54 is secured to the body 50 by a C-ring type locking ring 56.

1 Additionally, an external seal 58 is provided on the lower
portions of the latching mechanism 5 to provide sealing engage-
ment with the bore 2b of the production tubing string 2. Since
the latching mechanism 5 is entirely conventional, further
5 description thereof is believed unnecessary.

Latching mechanism 5 is provided at its bottom end
with external threads 59 which are respectively engaged by
internal threads provided on a connecting sub 212. Connecting
sub 212 is provided with external threads 214 which are thread-
10 ably engaged by internal threads formed on a seal retainer
sleeve 220. Seal retainer sleeve 220 traps an annular non-
elastomeric sealing element 216 between an upwardly facing
shoulder 222 formed on the seal retainer 220 and a downwardly
facing shoulder 213 formed on the connecting sub 212.

15 A conical valve head 102 forming part of a plug-type
valve unit 100 sealably engages the non-elastomeric seal element
216 to achieve a closing of the bore of the latching mechanism
5, thus closing the bore 5a of the production tubing string 2.
The conical valve head 102 is secured by internal threads 103
20 to the top end of a rod-like actuator 104, and actuator 104 is
spring biased by a spring 226 (Figure 2C) to the closed posi-
tion of the valve head 102 relative to the annular seal 216, as
will be later described in detail. A set screw 105 secures the
threaded engagement between valve head 102 and actuator rod
25 104. Below the annular seal 216, the seal retaining sleeve 220
is provided with a plurality of peripherally spaced, inclined,
radial ports 223 which provide for free communication between
the tubing casing annulus 1a and the bore 5a of latching mecha-
nism 5 when valve head 102 is shifted downwardly to its open
30 position, as shown in Figure 3B.

1 The lower end of seal retaining sleeve 220 is provided
with internal threads 218 which are secured to a tubular spring
housing 230 and secured by set screw 219. At its lower end,
the spring housing 230 mounts a C-type retaining ring 232
5 (Figure 2C) which in turn secures an annular abutment ring 234
in position to support the bottom end of a power spring 226.
Abutment ring 234 is provided with a plurality of axially
extending openings 235 to permit free fluid flow into the
annular chamber 238 defined between the inner wall of the
10 spring housing 230 and the external cylindrical surface of the
actuator rod 104. A top spring seat ring 106 abuts against a
downwardly facing shoulder 105 provided on the external surface
of the actuator rod 104. Spring seat 106 is engaged by the
upper end of the power spring 226 and is provided with a plura-
15 lity of axially extending apertures 108 to permit free fluid
flow from spring chamber 238.

A conventional internal seal and bearing structure
225 is mounted on the upper end of the spring housing 230 by
being positioned between an upwardly facing shoulder 231
20 provided on the inner surface of spring housing 230 and the
downwardly facing end surface of an annular plug 233 which is
secured to external threads 235 formed on the top inner surface
of the spring housing 230. Thus, the actuator rod 104 for the
valve unit 100 is slidably and sealably mounted in the tool for
25 axial movements relative to the annular valve seat 216 and is
held in a fail-safe closed position by the power spring 226.

The spring housing 230 is further provided at its
lower end with two sets of external threads 237 and 239.
(Figure 2C) External threads 237 cooperate with internal
30 threads formed on the top end of a main housing 250 and are

1 sealed by seal ring 241. The external threads 239 cooperate
with internal threads provided on the top end of a motor mounting
sleeve 240.

5 The motor mounting sleeve 240 extends downwardly a
substantial distance, and, at its bottom end, shown in Figure
2E, supports a fluid submersible reversible electric stepping
motor 260 which is only shown schematically. Motor 260 has an
externally projecting mounting flange 261 which is secured to
the motor mounting sleeve 240 by a plurality of peripherally
10 spaced, radially disposed bolts 242.

The output shaft 262 of the stepping motor 260 is
connected to the input shaft 272 of a conventional gear reduc-
tion unit 270 which has a peripherally extending mounting
flange 273 by which it is secured to the motor mounting sleeve
15 240 by a plurality of peripherally spaced bolts 244. Again,
this is a conventional unit and is only shown schematically.

The output shaft 274 of the gear reduction unit 270
is connected by a coupling sleeve 275 to the bottom end of an
externally threaded, axially extending screw element 280. A
20 conventional ball or roller bearing unit 276 mounts the screw
280 for rotation and the bearing unit 276 is secured to the
motor mounting sleeve 240 by a plurality of peripherally spaced
bolts 246.

The external threads 282 provided on the screw 280
25 cooperate in conventional fashion with threads, or preferably
balls, provided in a ball nut unit 290. Thus, rotation of the
screw 280 will produce an axial displacement of ball nut unit
290.

A guide sleeve 292 is secured to the top end of ball
30 nut unit 290 by threads 291. Guide sleeve 292 is provided with

1 a radially thickened portion 293 within which one or more keys
294 are mounted in a suitable recess 295. Keys 294 project
radially outwardly into a vertically extending slot 243 provided
in the wall of the motor mounting sleeve 240. Thus, the ball
5 nut 290 is secured against rotation and hence moves axially
when the screw 280 is rotated by motor 260.

The top end of the actuating sleeve 292 is provided
with internal threads 296 which engage external threads pro-
vided on the lower rod portion 112 of a force transmitting
10 collet 110. The upper end 113 of the collet 112 is of tubular
configuration and is provided with a plurality of peripherally
spaced, flexible arm portions 114, each of which terminates in
an inwardly enlarged head portion 116 (Figure 2C). The head
portions 116 are normally disposed below an external locking
15 rib 120 formed on the exterior of the actuating rod 104 when
such rod is in the closed position of the valve as shown in
Figure 2C. Upward movement of the collet 110 will produce an
engagement of the collet heads 116 with the locking rib 120 and
hence permit the actuating rod 104 to be pulled downwardly by
20 downward movement of the collet 110 produced by the actuating
sleeve 292, as shown in Figure 3D.

Immediately above the top end of the actuating sleeve
292, a fluid immersible, electric solenoid 130 is mounted.
Such solenoid is shown only schematically and is provided with
25 a ferromagnetic annular armature 132 which has an upwardly
extending sleeve portion 134 provided with internal threads
136. A latching sleeve 140 has external threads provided on
its bottom end cooperating with internal threads 136 and defines
an internally projecting, downwardly facing spring seat 143. A
30 relatively light compression spring 150 is compressed between

1 spring seat 143 and an external shoulder 115 provided on collet
110. Thus, the locking sleeve 140 and the armature 132 are
biased to an upward position relative to the solenoid 130.

When the solenoid 130 is energized, the armature 132 will be
5 shifted downwardly into engagement with the top end of such
solenoid and this downward axial movement of the latching
sleeve 140 moves a latching head 142 (Figure 2C) secured to the
top end of latching sleeve 140 into abutting engagement with
the outer walls of the collet arms 114, thus securing the col-

10 let locking heads 116 in engagement with the locking rib 120
provided on the actuating rod 104. This assumes, of course,
that the electric motor 260 has been energized to rotate first
in a direction to bring the collet latching heads 116 upwardly
to a position above the locking rib 120 on the actuator rod

15 104. It will be noted that a stop ring 107 is secured to the
external periphery of actuator rod 104 by set screws 109 to
limit the upward movement of the actuating collet 110. It
should also be noted that the solenoid 130 moves upwardly with
the collet 110, thus not affecting the position of the latching
20 sleeve 140 relative to the collet locking heads 116 until
solenoid 130 is energized.

The operation of that portion of the mechanism 11 of
the safety valve 10 heretofore described will be readily ap-
parent. Assuming that the safety valve is in its normal closed
25 position, the electric motor 260 is energized from a suitable
source of electricity, preferably a downhole battery, as will
be described, to move the collet 110 upwardly and thus position
the collet locking heads 116 above the locking rib 120 formed
on the actuator rod 104. When the motor stalls out due to
30 contact of the latching sleeve with the stop ring 107, an

1 electrical signal will be generated which will effect the
de-energization of the electric motor 260. The electric motor
260 is then energized to rotate in the opposite direction, thus
bringing the collet 110 downwardly and engaging the latching
5 heads 116 with the locking rib 120 on the actuator rod 104.
Concurrently therewith, the solenoid 130 is energized, thus
moving the ferromagnetic armature 132 downwardly and effecting
a downward displacement of the latching sleeve 140 relative to
the collet 110 to bring the latching head 142 into abutting
10 engagement with the collet locking heads 116, thus securing the
locking heads to the actuator rod 104 and assuring that the
actuator rod 104 will be moved downwardly to the open position
shown in Figure 3D. The electric motor 260 may be de-energized
without affecting the position of the actuator rod 104 since it
15 is locked in position by the locking sleeve 140. Subsequent
de-energization of the solenoid 130 will permit the armature 132
to be moved upwardly by the spring 150 and this will move the
latching head 142 out of abutting engagement with the collet
locking heads 116, permitting such collet locking heads to
20 release from the locking rib 120 on the actuator rod 104, hence
permitting the actuator rod 104 to be driven upwardly by the
power spring 226 to return the valve head 102 to its closed,
sealed position with respect to the annular seal 216.

25 In the preferred embodiment of the invention, the
energization and de-energization of the electric motor 260 and
the latching solenoid 130 are respectively controlled by
electromagnetic wave signals transmitted from a surface trans-
mitter and received by the downhole antenna 16. Figures 2E,
2F, 2G, 2H, 2I, 2J, 2K and 2L indicate the preferred apparatus
30 for effecting the energization and control of these downhole

1 electrical elements. To minimize friction, and to provide a
noncorrosive environment, the motor 260, the gear box 270, the
ball nut screw 280, the ball nut 290 and all of the valve
actuating structure thereabove, up to the seal unit 225 (Figure
5 2B), are preferably surrounded with an appropriate oil having
both lubricating and insulating properties. A seal 256 (Figure
2F) at the bottom of main housing 250 and seal 241 (Figure 2C)
at the top of main housing 250 cooperate with seal assembly 225
to provide a chamber for such oil which may be inserted through
10 a plugged hole (not shown). Such oil will undergo a substantial
expansion due to temperature change as the mechanism is lowered
into the well. For this reason, a pressure compensating cylinder
300 (Figure 2E) is mounted in the lower end of the main housing
250. Cylinder 300 has an upper end cap 302 secured thereto by
15 threads 303 and having a plurality of axially extending holes
304 extending therethrough to permit the lubricating fluid to
freely enter the interior of the pressure equalizing cylinder
300. A conventional piston 306 is slidably and sealably mounted
within the bore of the pressure compensating cylinder 300. The
20 lower end of cylinder 300 has a pipe 310 (Figure 2F) sealably
secured thereto and communicating with a bore 322 provided in a
connecting sub 320, which bore extends to the casing annulus
1a. Since the connecting sub 320 is threadably secured to
internal threads 254 provided in the bottom end of main housing
25 250 and the threaded connection is sealed by seal 256, it will
be apparent that any increase in fluid pressure within the
space defined by the main housing 250 will result in a downward
displacement of the pressure compensating piston 306 and the
pressure is relieved by exhausting well fluid below the piston
30 306 through the conduit 322 to the casing annulus.

1 A conventional threaded and sealed connection
mechanism 330 is provided between the bottom end of the con-
necting sub 320 and the top end of a tubular battery module
340. The batteries are not shown in the drawings.

5 The bottom end of battery module 340 is threadably
and sealably connected through a conventional connecting mech-
anism 350 to the top end of an electronic module 360 which
contains the receiver, central processor, motor controller and
driver schematically shown in the circuit diagram of Figure 4.

10 The bottom end of the electronics module 360 is
provided with an end cap 362 and such end cap is connected by a
conventional flexible or universal joint 370 to the top end of
a housing 402 forming part of a stabilizer unit 400. Stabilizer
unit 400 is shown and described in detail in co-pending applica-
15 tion **GB 8905150** filed concurrently herewith and
assigned to the assignee of the instant invention. Such disclo-
sure is hereby incorporated in this application by reference
and will not be described in detail. In the run-in position of
the stabilizer unit 400, a plurality of peripherally spaced,
20 radially expandable linkages 406 are provided on housing 402.
Each linkage 406 mounts a pair of axially spaced anti-friction
rollers 404 which are held in a radially retracted position as
shown in Figure 2H, during run-in. Such linkage is expanded to
a radially expanded position by the melting of a fusible pin
25 408 which is meltable when exposed to the well temperatures
existing at the depth of insertion of the safety valve 10.
When pin 408 melts, the rollers 404 move out to a radially
expanded position under the bias of spring 410 and engage the
bore wall of the well casing 1, as shown in Figure 3H.

1 The bottom end of stabilizer housing 402 is threadably
and sealably secured through a conventional connection mechanism
450 to the top end of a tubular antenna module 500 in which the
dipole antenna 16 (Figure 4) is conventionally mounted.

5 The bottom end of antenna module 500 is threadably
and sealably connected to the top end of a second stabilizer
unit 400 which is identical to the upper stabilizer unit 400
previously described. Thus, both ends of the antenna module
500, when the stabilizer units have been radially expanded, are
10 held in a rigid position in exact concentric relationship to
the axis of the well conduit 1. Through the use of the two
axially spaced stabilizer units 400, it is thereby assured that
fluctuations in fluid velocity passing the exterior of the
antenna module 500 will not produce any form of vibration of
15 such module, thus eliminating the possibility of generation of
a noise signal which would interfere with the control signals
transmitted to the antenna 16 from a surface transmitter 18, as
shown by the schematic circuit diagram of Figure 4.

20 Referring now to Figure 5, there is shown a modified
safety valve embodying this invention which incorporates a
pressure equalizing feature. Those skilled in the art will
recognize that it is desirable that the fluid pressures ex-
isting above and below the valve head be equalized prior to
effecting axial movement of the valve head relative to the
25 annular seal. In Figure 5, where similar numerals indicate
parts similar to those previously described, the conical valve
head 500 is not directly connected to the actuating rod 104 as
in the previously described modification. Instead, the con-
nection of valve head 500 is effected through a lost motion
30 connection.

1 Thus, a lost motion connecting sleeve 510 is thread-
ably secured to threads 103 on the top end of the actuator rod
104. Lost motion connecting sleeve 510 has an internally
projecting rib 512 at its upper end which is engagable with an
5 external rib 522 formed on a valve plug 520 which, in the
closed position of the valve head 500 closes a small central
bore 501 formed in such valve head. Valve plug 520 is urged to
a closing position by a compression spring 530 which is com-
pressed between the valve plug 520 and the top end of actuator
10 rod 104. The lost motion connecting sleeve 510 is provided
with an external rib 514 which, after limited downward movement
of the actuator rod 104 sufficient to pull the valve plug 520
out of the bore 501 of the valve head 500 engages an internally
projecting shoulder 542 formed on the end of a sleeve 540 which
15 is secured to external threads 502 formed on the lower portion
of the valve head 500. Additionally, the valve head 500 is
provided with one or more radial passages 526 which provide a
fluid connection between the valve head bore 501 and the casing
annulus 1a through the inclined radial passages 223.

20 The operation of this modification of the invention
will be readily understood by those skilled in the art. In the
closed position of the valve illustrated in Figure 5A, the bore
501 of the valve head 500 is closed by the valve plug 520 which
is urged to its closed position by the compression spring 530.
25 Initial downward movement of the actuator rod 104 will pull the
valve plug 520 downwardly by lost motion sleeve 510 to open the
bore 501 to fluid flow to the casing annulus, thus equalizing
the fluid pressures above and below the valve head 500 before
the valve head 500 is moved from its sealing engagement with
30 the annular seal ring 216. Further downward movement of the

actuating rod 104 will bring the external shoulder 514 on the connecting sleeve 510 into engagement with the internally projecting shoulder 542 on the sleeve 540 and effect downward movement of the valve head 500, thus completely opening the bore of the tubing string to communication with the casing annulus, as shown in Figure 5B.

From the foregoing description, it will be readily apparent to those skilled in the art that this invention provides a unique mechanism for effecting the shifting of a safety valve, spring biased to a closed position, to an open position by a downhole electric motor energized by downhole batteries. The invention also provides a solenoid actuated latching mechanism for locking the safety valve in an open position, thus eliminating current drain on the batteries except for that required to hold the solenoid actuated latch in its collet engaging position. The current drain on the downhole batteries is thus significantly reduced.

It is also readily apparent that a surface source of electricity could be employed to effect the energization and de-energization of the downhole motor and the latching solenoid, and the invention is not to be construed as limited to use with a downhole battery as the source of energy.

CLAIMS

1. Apparatus for shifting a downhole tool axially shiftably mounted in a subterranean well conduit for movement between an initial and a second position
5 comprising,
 an axially extending actuator connected at one end to the downhole tool;
 resilient means opposing axial movement of the actuator in the direction away from the initial position;
10 peripheral abutment means on the actuator;
 shifting means disposed adjacent the actuator;
 an axial force transmitting member in operative engagement with the shifting means;
 means for mounting the force transmitting member for
15 non-rotatable axial movement relative to the conduit;
 an electric motor fixedly mounted in the conduit;
 and threaded means rotatable by the electric motor and threadably engageable with the force transmitting member to axially shift the shifting means and the
20 actuator in the direction opposed by the resilient means and thereby position the downhole tool in the second position.
2. An apparatus according to claim 1 wherein the downhole tool comprises a valve having an open and a
25 closed position relative to the bore of the well conduit and the resilient means oppose movement of the valve from the closed position.
3. An apparatus according to claim 2 further comprising means for equalizing fluid pressure across the valve
30 prior to moving the valve from the closed position.
4. An apparatus according to any of claims 1 to 3 further comprising downhole battery means for supplying power to said electric motor; and electromagnetic wave means, including a transmitter exterior of the apparatus,
35 for controlling the energization of said electric motor.

5. An apparatus according to any of claims 1 to 4 in which the shifting means comprise a collet having a ring portion and a plurality of peripherally spaced resilient arm portions disposed adjacent the actuator and that have enlarged head portions engageable with the peripheral abutment means to impart an axial force to the actuator to axially shift the tool in the direction opposed by the resilient means and the axial force transmitting member is secured to the collet ring portion.
- 10 6. An apparatus according to any preceding claim further comprising
- a latch sleeve that is axially movable relative to the well conduit and taht has locking surfaces movable to a position in engagement with said shifting means to
- 15 retain the shifting means in locked position;
- electromagnet means for axially shifting the latch sleeve from a remote position relative to the shifting means to the position retaining the shifting means in locked position;
- 20 and control circuit means operable from exterior of the apparatus for controlling the direction and extent of rotation of the electric motoro and the energization and de-energization of the electromagnet means, whereby the downhole tool is moved by the electric motor to the
- 25 second position by energization of the electromagnet means and returned by the spring to the initial position by de-energization of the electromagnet means.
7. An apparatus according to claims 5 and 6 in which the locking surfaces are movable to a position in
- 30 engagement with the enlarged head portions of the collet to retain the collet head portions in locked position.
8. An apparatus according to claim 6 or claim 7 further comprising downhole battery means for supplying power to the electric motor and the electromagnet means; and
- 35 electromagnetic wave means for selectively controlling

the energization of the electric motor and the electromagnet means and that include a transmitter exterior of the apparatus.

9. An apparatus according to claim 8 further comprising
5 an antenna fixedly mounted in a portion of the well conduit, and means for stabilising the well conduit portion in the well bore to prevent vibration thereof.

10. An apparatus according to any of claims 1 to 5
10 further comprising tubular housing means sealably enclosing the shifting means, the axial force transmitting member, the electric motor and the threaded means; and means for filling the housing means with a lubricating fluid.

11. An apparatus according to any of claims 6 to 9
15 further comprising tubular housing means sealably enclosing the shifting means, the axial force transmitting member, the latch sleeve, the electromagnetic means, the electric motor and the threaded means; and means for filling the housing means
20 with a lubricating fluid.

12. An apparatus according to claim 10 to claim 11
further comprising a fluid expansion chamber communicating with the bore of the tubular housing means to accommodate thermal expansion of fluid contained in
25 the tubular housing.

13. An apparatus according to any of claims 6 to 9 in which the control circuit means are operable from the well surface.

14. The method of axially shifting a downhole tool in a
30 subterranean well from an initial position to a second position against the bias of a spring comprising the steps of:

axially shifting the downhole tool to the second position by an electric motor driven gearing mechanism;

supplying power to said electric motor from a downhole battery;

latching the downhole tool in said second position by a solenoid shiftable latch energized by said downhole
5 battery, whereby said downhole tool remains in said second position without energization of said electric motor; and

selectively controlling the energization of said electric motor and said solenoid by electromagnetic wave
10 signals transmitted through the earth.

15. The method of claim 14 wherein said downhole tool is a valve having an initial closed position and a second open position.

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